

METHOD AND APPARATUS FOR IMAGE SQUARENESS CORRECTION

BACKGROUND OF THE INVENTION

[0001] Printing systems utilizing a Raster Output Scanning (ROS) device to form images on a photoreceptor surface are well known in the art. Conventionally, the ROS includes a diode or gas laser for generating a coherent beam of radiation, a modulator for modulating the laser output in accordance with an input video image signal, and a multifaceted polygon scanner for scanning the modulated laser beam output line by line across the surface of the photoreceptor to form the latent image. Also included in the ROS are various optical components to collimate, expand, focus, and align the modulated scanning beams. These optical components are fixedly mounted within a housing frame, which is positioned within a printer machine frame, so that the modulated and shaped scanning beams emerging from a window in the housing are directed perpendicular to the photoreceptor surface to form scan lines. The lines will be formed in parallel across the surface of the photoreceptor belt. The belt should be aligned so that these parallel lines are formed perpendicular to the direction of belt travel. It is difficult to achieve this perpendicularity, resulting in a condition referred to as "scan line skew" causing a squareness error, wherein the image effectively takes the form of a parallelogram. This condition will affect the images which are subsequently developed and transferred to output prints, the output prints exhibiting degradation of quality due to the skew effects.

[0002] In the past, the ROS would be adjusted manually until the squareness error was eliminated, however, newer systems provide stepper motor driven ROS de-skew mechanisms. For example, in U.S. Patent Number 5,374,993 an adjustment example is provided that requires a multi-step procedure of printing a test pattern, determining a registration edge skew introduced by the paper feed path, determining a lead edge skew, subtracting the registration edge skew from the

20200520001

lead edge skew to determine the scan line skew, loosening a clamp securing the ROS housing, determining the number of hex flat increments required to correct the scan line skew from a table, turning an adjustment screw by the indicated number of hex screw flat increments, and re-tightening the clamp securing the ROS housing.

SUMMARY OF THE INVENTION

[0003] A method of correcting output image squareness in a laser printer system having a Raster Output Scanning (ROS) device with a pivotal mounting is provided. The method includes printing a test pattern that includes at least three markers such as crosshairs positioned in a predetermined geometric arrangement, measuring a plurality of distances between markers and calculating a skew angle based on the measured distances. In a preferred embodiment, the markers are printed in a rectangular arrangement and the skew angle is calculated using the Law of Cosines. The ROS device is then automatically rotated by an amount sufficient to correct the skew angle. The ROS rotation is performed automatically by an adjustment system connected to the ROS. The method optionally includes a scanner for scanning the test pattern image and making the measurements automatically via a program configured to analyze the scanned image.

BRIEF DESCRIPTION OF THE DRAWINGS

[0004] FIGURE 1 is a representation of a ROS housing adjustably seated over a photoreceptor belt;

[0005] FIGURE 2 shows a test pattern print output used to determine scan line skew;

[0006] FIGURE 3 shows a skewed test print output and measurements;

[0007] FIGURE 4 depicts correction of ROS skew during registration setup of a laser printer system; and

[0008] FIGURE 5 shows an alternate skewed test print output and measurements.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

[0009] Referring to FIGURE 1, there is shown an exemplary representation of a printer section 10 of a laser based printing system having an adjustable ROS housing 12 pivotally mounted at a pivot point 14 and having a ROS arm 16 and ROS ball 18 on the side opposite to the pivot point 14. The ROS ball 18 docks in a notch 20 in a solid block 22. A pair of flexible springs 24 and 26, formed in the shape of a flat ribbon, are fixedly mounted to the solid block 22 and to a frame surface 28. As viewed in FIGURE 1, only the edges of the springs 24 and 26 are visible. The springs 24 and 26 hold the block 22 against a cam 30 so that the cam 30 can rotate the ROS housing 12 about the pivot point 14. The solid block 22, flexible springs 24 and 26, cam 30 and a stepper motor 32 form an adjustment system wherein the cam 30 is driven by the stepper motor 32 so that the process of rotating the ROS housing 12 can be automated electronically.

[0010] It is to be appreciated that other arrangements and devices can be utilized for automating adjustment of the ROS housing 12 electronically, and that these other devices and arrangements fall within the scope of the present invention.

[0011] As viewed from the perspective of FIGURE 1, ROS housing 12 is positioned above a photoreceptor belt 34, and the ROS housing may include a laser, modulator, polygon scanner, and other optical elements required to focus and direct output beams which are in turn scanned across the moving photoreceptor belt 34. Image lines are exposed at the photoreceptor belt 34 with each scan to create a latent electrostatographic image 36 of the document being imaged. The latent image 36 can then be developed and transferred to a copy sheet with the transferred image being fused. This process is well known to persons of average skill in the art. If the photoreceptor belt 34 is skewed in the process direction, however, the

scanned line 38 will not be perpendicular to the belt edges or parallel to the lead edge of the images in the process direction. The scan line 38 will vary from the desired perpendicular direction by a skew angle 40, referred to hereinafter as angle ϕ . The resulting output prints will exhibit copy quality defects resulting from the scan line skew.

[0012] According to the present invention, the ROS housing 12 is mounted within printer section 10 in such a way as to enable adjustment of the housing components to compensate for the housing-to-belt skew angle ϕ .

[0013] As previously described, ROS housing 12 is pivotally mounted at a pivot point 14 and having a ROS arm 16 and ROS ball 18 on the side opposite to the pivot point 14. The ROS ball 18 docks in a notch 20 in a solid block 22. A pair of flexible springs 24 and 26, formed in the shape of a flat ribbon, are fixedly mounted to the solid block 22 and to a frame surface 28. The block 22 is, therefore, held in contact with the cam 30 which can rotate the ROS housing 12 about the pivot point 14 by moving the block 22 in the desired direction to reduce skew angle ϕ . For example, in one embodiment, the cam 30 can be configured so that rotating the cam in a clockwise direction from an initial position will cause ROS housing 12 to rotate in a counterclockwise direction, thereby numerically increasing skew angle ϕ , wherein a preferred value of zero is represented by a dashed line 42. Similarly, rotating the cam in a counterclockwise direction from an initial position will cause ROS housing 12 to rotate in a clockwise direction, thereby numerically reducing skew angle ϕ .

[0014] In prior art environments, the ROS would be manually adjusted until the squareness error, skew angle ϕ , was eliminated. In the present embodiment, however, with a stepper motor driven ROS de-skew mechanism, the adjustment of the ROS angle 44, hereinafter referred to as ROS angle θ , is automated. A system and process is therefore described herein for determining the skew angle ϕ

utilizing measured linear distances, and using those measurements as input for adjusting the ROS angle (θ) **44** to a preferred value of 90 degrees by reducing the magnitude of skew angle ϕ to substantially zero. In the embodiment described herein, three linear distances are utilized, however, other embodiments may use as few as two linear distances.

[0015] A first step in measuring skew angle ϕ is to print a test pattern of markers, such as cross hatches for example. FIGURE 2 shows a test pattern **46** suitable for use in the present embodiment. Cross hatches **48**, **50**, **52** and **54** are printed such that they form the four corners of a rectangle. Rather than measuring the skew angle ϕ , or the complementary ROS angle θ , directly, it is more convenient and accurate to measure the distances between three pairs of the cross hatches as illustrated. The measured distances are labeled a (**56**), b (**58**) and c (**60**) in FIGURE 2. Distance **56** represents a horizontal distance, distance **58** represents a vertical distance, and distance **60** represents a diagonal distance.

[0016] Referring now to FIGURE 3 which shows an exemplary printed test pattern having a nonzero skew angle ϕ , and with continuing reference to FIGURES 1 and 2, a procedure of determining ROS angle θ and skew angle ϕ is now described. Since ROS skew does not affect the angle of the line connecting the leftmost two crosshairs **48**, **52** (distance b), it follows that $\phi = \pi/2 - \theta$. Using the Law of Cosines, θ can be solved for with

$$\theta = \cos^{-1} \left(\frac{a^2 + b^2 - c^2}{2ab} \right) \quad (1)$$

and hence

$$\phi = \frac{\pi}{2} - \cos^{-1} \left(\frac{a^2 + b^2 - c^2}{2ab} \right) \quad (2)$$

or

$$\phi = \sin^{-1} \left(\frac{a^2 + b^2 - c^2}{2ab} \right) \quad (3)$$

10-1	100
10-2	100
10-3	100
10-4	100
10-5	100
10-6	100
10-7	100
10-8	100
10-9	100
10-10	100
10-11	100
10-12	100
10-13	100
10-14	100
10-15	100
10-16	100
10-17	100
10-18	100
10-19	100
10-20	100
10-21	100
10-22	100
10-23	100
10-24	100
10-25	100
10-26	100
10-27	100
10-28	100
10-29	100
10-30	100
10-31	100
10-32	100
10-33	100
10-34	100
10-35	100
10-36	100
10-37	100
10-38	100
10-39	100
10-40	100
10-41	100
10-42	100
10-43	100
10-44	100
10-45	100
10-46	100
10-47	100
10-48	100
10-49	100
10-50	100
10-51	100
10-52	100
10-53	100
10-54	100
10-55	100
10-56	100
10-57	100
10-58	100
10-59	100
10-60	100
10-61	100
10-62	100
10-63	100
10-64	100
10-65	100
10-66	100
10-67	100
10-68	100
10-69	100
10-70	100
10-71	100
10-72	100
10-73	100
10-74	100
10-75	100
10-76	100
10-77	100
10-78	100
10-79	100
10-80	100
10-81	100
10-82	100
10-83	100
10-84	100
10-85	100
10-86	100
10-87	100
10-88	100
10-89	100
10-90	100
10-91	100
10-92	100
10-93	100
10-94	100
10-95	100
10-96	100
10-97	100
10-98	100
10-99	100
10-100	100

[illegible]

10-1	100
10-2	100
10-3	100
10-4	100
10-5	100
10-6	100
10-7	100
10-8	100
10-9	100
10-10	100
10-11	100
10-12	100
10-13	100
10-14	100
10-15	100
10-16	100
10-17	100
10-18	100
10-19	100
10-20	100
10-21	100
10-22	100
10-23	100
10-24	100
10-25	100
10-26	100
10-27	100
10-28	100
10-29	100
10-30	100
10-31	100
10-32	100
10-33	100
10-34	100
10-35	100
10-36	100
10-37	100
10-38	100
10-39	100
10-40	100
10-41	100
10-42	100
10-43	100
10-44	100
10-45	100
10-46	100
10-47	100
10-48	100
10-49	100
10-50	100
10-51	100
10-52	100
10-53	100
10-54	100
10-55	100
10-56	100
10-57	100
10-58	100
10-59	100
10-60	100
10-61	100
10-62	100
10-63	100
10-64	100
10-65	100
10-66	100
10-67	100
10-68	100
10-69	100
10-70	100
10-71	100
10-72	100
10-73	100
10-74	100
10-75	100
10-76	100
10-77	100
10-78	100
10-79	100
10-80	100
10-81	100
10-82	100
10-83	100
10-84	100
10-85	100
10-86	100
10-87	100
10-88	100
10-89	100
10-90	100
10-91	100
10-92	100
10-93	100
10-94	100
10-95	100
10-96	100
10-97	100
10-98	100
10-99	100
10-100	100

[illegible][illegible]

configured with a program to automatically calculate distances a, b and c, and then to rotate the cam **30** in a direction and angular displacement sufficient to reduce the magnitude of skew angle ϕ to substantially zero.

[0019] The procedure depicted in FIGURE 4 can eliminate skew error in a single step, however, the procedure may be repeated one or more times to confirm correct angular positioning of the ROS housing **12**. It is also to be appreciated that, in the above-described process and an alternative process described below, the method of measuring and correcting scan line skew is independent of any registration edge skew produced by the paper feed mechanism. In the past, such as in the aforementioned U.S. Patent Number 5,374,993, it was necessary to subtract the registration edge skew from a lead edge skew to arrive at the scan line skew.

[0020] An exemplary test pattern measurement and calculation of skew angle ϕ is provided here to demonstrate the use of Equation 3:

$$\begin{aligned}a &= 8 \text{ in.}, \\b &= 6 \text{ in.}, \\c &= 9.95 \text{ in. and} \\ \phi &= 0.595 \text{ degrees.}\end{aligned}$$

[0021] Another exemplary test pattern measurement and calculation of skew angle ϕ is provided here to demonstrate an adjustment in a direction opposite to that of the first example wherein the resultant angle is negative in value:

$$\begin{aligned}a &= 8 \text{ in.}, \\b &= 6 \text{ in.}, \\c &= 10.05 \text{ in. and} \\ \phi &= -0.598 \text{ degrees.}\end{aligned}$$

[0022] After printer system **62** adjusts the angular position of the ROS housing **12** for either of the two examples above, the preferred results of a second test would yield:

a = 8 in.,
b = 6 in.,
c = 10 in. and
 $\phi = 0$ degrees.

[0023] While the embodiment described above utilizes a test pattern **46** having four rectangularly positioned crosshatches, it is to be understood that other known predetermined geometric shapes may be used requiring as few as two distance measurements. For example, FIGURE 5 shows a test pattern **70** having three crosshatches **72**, **74** and **76** printed in the arrangement of an isosceles triangle. In this exemplary case, any two of distances labeled a, b and c (**78**, **80**, **82**) are measured. These distances respectively represent the measured lengths of the base, left and right legs of the skewed isosceles triangle **70**. The scan line skew is given by any one of the following equations depending on the choice of distances measured:

$$\phi = \sin^{-1} \left[\left(\frac{b^2}{a^2} - 1 \right) \left(\frac{1}{\cos 30^\circ} \right) \right] \quad (4)$$

$$\phi = \sin^{-1} \left[\left(1 - \frac{c^2}{a^2} \right) \left(\frac{1}{\cos 30^\circ} \right) \right] \quad (5)$$

$$\phi = \sin^{-1} \left[\left(\frac{b^2 - c^2}{b^2 + c^2} \right) \left(\frac{1}{\cos 30^\circ} \right) \right] \quad (6)$$

where ϕ represents skew angle **40** as shown.

[0024] Exemplary test pattern measurements representing positive and negative values of skew angle ϕ are provided here to demonstrate the use of Equation 4:

a = 6 in.,
b = 6.0452 in.,
c = 5.9545 in.,
 $\phi = 1$ degree,

and

$$a = 6 \text{ in.},$$

$$b = 5.9545 \text{ in.},$$

$$c = 6.0452 \text{ in.},$$

$$\phi = -1 \text{ degree},$$

where ϕ is calculated using any one of Equations 4, 5 or 6 utilizing the respective two of distances a, b and c.

[0025] While the invention has been described with respect to specific embodiments by way of illustration, many modifications and changes will occur to those skilled in the art. It is therefore, to be understood that the appended claims are intended to cover all such modifications and changes which fall within the true spirit and scope of the invention.